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Design of FIR Filters:

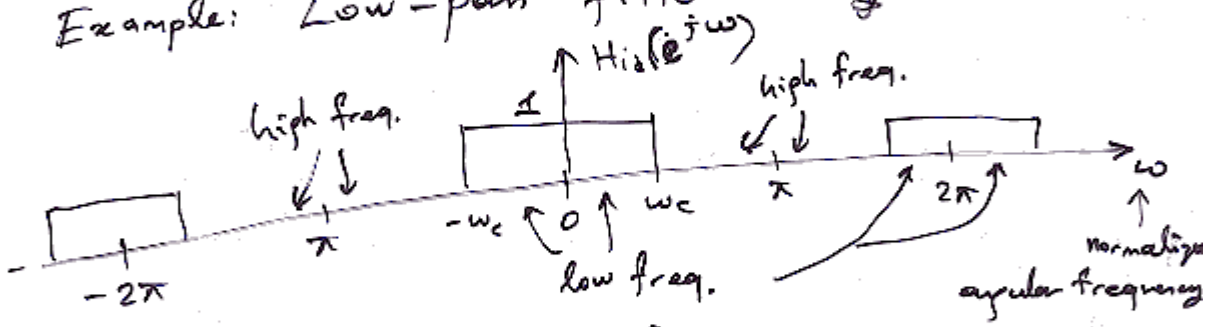
FIR filter: $y[n] = \sum_{k=0}^{M-1} h[k] x[n-k]$ Causal FIR.

$y[n] = \sum_{k=0}^{M-1} a_k x[n-k]$ where $h[k] = a_k$.

Anticausal FIR: $y[n] = \sum_{k=-L}^L b_k x[n-k] \Rightarrow h[k] = b_k, k=0, \pm 1, \dots, \pm L$. Impulse resp.

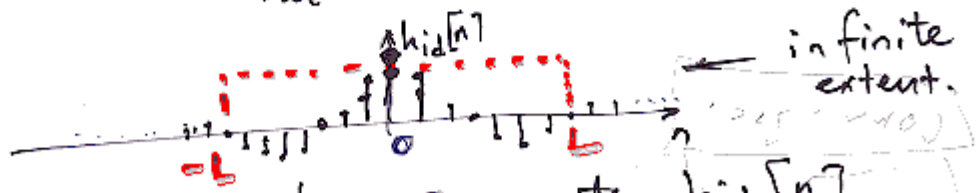
Design problem: Find the impulse response $h[n]$ satisfying some requirements.

Example: Low-pass filter design.



$$h_{id}[n] = \frac{1}{2\pi} \int_{-\pi}^{\pi} H_{id}(e^{j\omega}) e^{j\omega n} d\omega$$

$$h_{id}[n] = \frac{1}{2\pi} \int_{-\omega_c}^{\omega_c} e^{j\omega n} d\omega = \frac{\sin(\omega_c n)}{\pi n}, n=0, \pm 1, \pm 2, \dots$$



Possible approach: Truncate $h_{id}[n]$ \leftarrow FIR anticausal.

$$h_T[n] = \begin{cases} h_{id}[n], & n=0, \pm 1, \dots, \pm L \\ 0, & \text{otherwise} \end{cases}$$

2nd Approach: Least Squares Approach. [2] 28 Subtotal

minimizing $\frac{1}{2\pi} \int_{-\pi}^{\pi} |H_L(e^{j\omega}) - H_{id}(e^{j\omega})|^2 d\omega = \sum_{n=-\infty}^{\infty} |h_L[n] - h_{id}[n]|^2$

freq. resp. of the filter.

$$= \sum_{n=-L}^L |h_L[n] - h_{id}[n]|^2 + \sum_{n=L+1}^{\infty} |h_{id}[n]|^2 + \sum_{n=-\infty}^{-L+1} |h_{id}[n]|^2$$

Equivalent minimization problem

$$\min \sum_{n=-L}^L (h_L[n] - h_{id}[n])^2 = B$$

↑ real
↑ known
↑ real

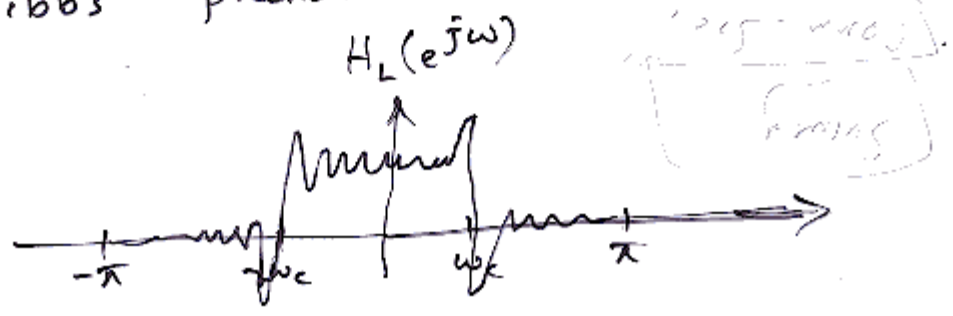
$$\frac{\partial B}{\partial h_L[k]} = 0, \quad k=0, \pm 1, \pm 2, \dots, \pm L.$$

$$= 2(h_L[k] - h_{id}[k]) + \sum_{n \neq k} 2(h_L[n] - h_{id}[n]) \cdot 0$$

$$\Rightarrow h_L[k] = \begin{cases} h_{id}[k], & k=0, \pm 1, \pm 2, \dots, \pm L \\ 0, & \text{otherwise} \end{cases}$$

* This design method produced nothing new! \Rightarrow Rectangular window design.

* Gibbs phenomenon.



Window-based FIR Filter Design:

$$h_w[n] = h_{id}[n] \cdot w[n]$$

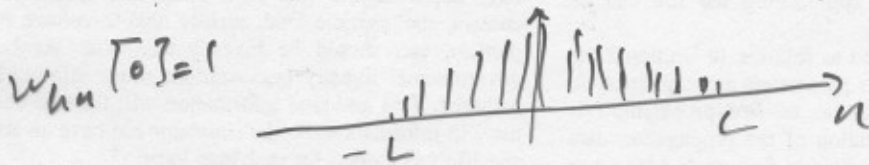
where $w[n]$ is a window of length $2L+1$ and centered around $n=0$. ($h_{id}[n]$ is symmetric w.r.t $n=0$ for lowpass, highpass & bandpass filters)

Example: Hanning window:

$$\rightarrow w_{hn}[n] = \frac{1}{2} + \frac{1}{2} \cos\left(\frac{2\pi n}{M-1}\right)$$

$$M = 2L+1$$

$$n = -L, \dots, 0, \dots, L$$



~~Blackman~~ Hamming window: $w_h[n] = 0.54 + 0.46 \cos\left(\frac{2\pi n}{M-1}\right)$
 $w_h[0] = 1$

Triangular window:

The one with $w_T[-L] = 0$

$w_T[-(L+1)] = 0$
 $w_T[L] \neq 0$
 (Bartlett)

Blackman window: $w_b[n] = 0.42 - 0.5 \cos\frac{2\pi n}{M-1} + 0.08 \cos\frac{4\pi n}{M-1}$
 (causal)

	transition width of mainlobe	Peak sidelobe is	
rect	$4\pi/2L+1$	-13dB	below the main lobe
Bartlett	$8\pi/2L+1$	-27dB	" " "
Hanning	$8\pi/2L+1$	-32dB	" " "

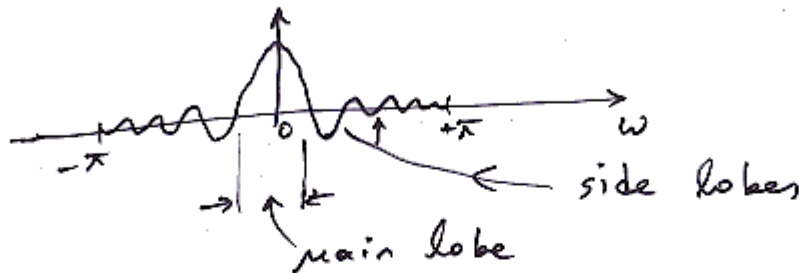
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Assume the Window is rectangular.

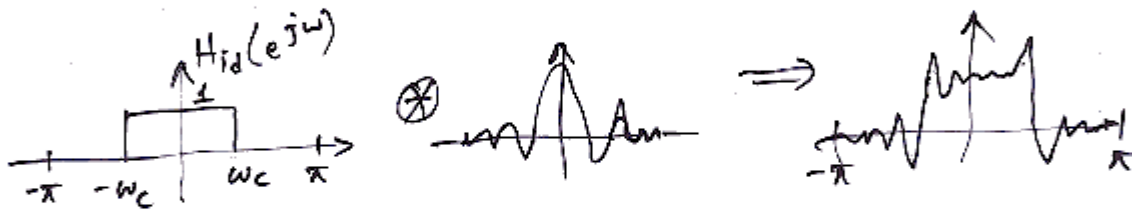
$$W_r(e^{j\omega}) = \sum_{n=-L}^L 1 \cdot e^{-jn\omega}$$

$$= 1 + e^{j\omega} + e^{-j\omega} + e^{j2\omega} + e^{-j2\omega} + \dots + e^{jL\omega} + e^{-jL\omega}$$

$$W_r(e^{j\omega}) = 1 + 2(\cos \omega + \cos 2\omega + \dots + \cos L\omega)$$



As $L \uparrow$ width of main lobe decreases.



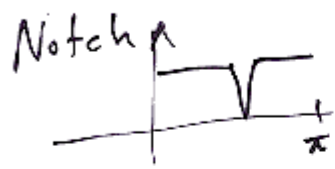
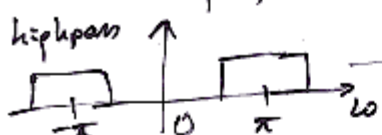
Type of window	Approximate transition width of main lobe	peak sidelobe (dB)
Rectangular	$4\pi / (2L+1)$	-13
(triangle) Bartlett	$8\pi / (2L+1)$	-27
Hanning	$8\pi / (L+1)$	-32
Hamming	$8\pi / (L+1)$	-43
Blackman	$12\pi / (2L+1)$	-58

Wider main lobe \Rightarrow slow transition from passband to stopband!
 (If $W(e^{j\omega}) = \delta(\omega) \Rightarrow$ instant transition.)

lower peak side lobe \Rightarrow Reduced Gibbs effect!

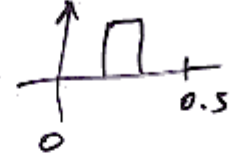
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* Highpass, band pass, Notch, band stop



$\mathcal{F}^{-1} \rightarrow h_{hp}[n] \rightarrow w[n]h_{hp}[n] = h_d[n]$

in some books



* ~~Anti~~ Causal filter design.
 $\Rightarrow h_d[n]$ is ^{infinite extent.} (anticausal symmetric wrt. 0) in all of the above filters.

$h_c[n] = w[n] \cdot h_d[n] \Rightarrow$ Anticausal.
 Filter order $2L+1$.

Causal

$h_c[n] = h_d[n-L]$

$h_d[n] = \{h_d[-L], \dots, h_d[0], \dots, h_d[L]\}$

$h_c[n] = \{h_d[-L], \dots, h_d[0], \dots, h_d[L]\}$
 (with $n=0$ under $h_d[-L]$ and $n=2L+1$ under $h_d[L]$)

Filter order $M = 2L+1$ odd!

$H_c(e^{j\omega}) = H_d(e^{j\omega}) e^{-j\omega L}$ ← linear phase term.

$|H_c(e^{j\omega})| = |H_d(e^{j\omega})|, |e^{j\omega L}| = 1$

$\phi_c(e^{j\omega}) = -\omega L$

Zero phase design: "Anticausal design"

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In Oppenheim Windows are defined for

Causal filters: e.g. Blackman : $w_{bl}[n] = 0.42 - 0.5 \cos\left(\frac{2\pi n}{M-1}\right) + 0.08 \cos\left(\frac{4\pi n}{M-1}\right)$
 $n=0, 1, \dots, M-1$

Hanning : $w_{hn}[n] = \frac{1}{2} \left(1 - \cos\left(\frac{2\pi n}{M-1}\right)\right)$

Filter order: M ? ($M \approx 2L+1$)

higher $M \uparrow \rightarrow$ better approximation.
 \rightarrow computational cost increases

* One may need to design filters with several M values and check the frequency response until it is satisfactory!

* Kaiser's formula for estimating M :

$$M = \frac{-20 \log_{10}(\sqrt{\delta_1 \delta_2}) - 13}{14.6 (\omega_s - \omega_p) / 2\pi} + 1$$



passband transition band stop-band

transition band: don't care region.

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General rules:

- * Narrow transition $(\omega_s - \omega_p) \downarrow \Rightarrow M \uparrow$
- * $\delta_1, \delta_2 \downarrow \Rightarrow M \uparrow$
- * $M \uparrow \Rightarrow$ high computational load.

* Ex Design a highpass from a lowpass:



= high pass filter: with cut off ω_c

$$H_{hp}(e^{j\omega}) = 1 - H_{lp}(e^{j\omega})$$

$$h_{hp}[n] = \delta[n] - h_{lp}[n]$$

Ex $h_{lp}[n] = \left\{ \frac{1}{4}, \frac{1}{2}, \frac{1}{4} \right\}$

$$h_{hp}[n] = \left\{ \underset{\uparrow n=0}{1} \right\} - \left\{ \frac{1}{4}, \underset{\uparrow n=0}{\frac{1}{2}}, \frac{1}{4} \right\} = \left\{ \underset{\uparrow n=0}{-\frac{1}{4}}, \frac{1}{2}, -\frac{1}{4} \right\}$$